

3.2 Cubic Bézier Curves

Ex 3.3

$$\begin{aligned} X(t) &= \begin{bmatrix} x \\ y \end{bmatrix} = \begin{bmatrix} -(1-t)^3 + t^3 \\ 3(1-t)^2t - 3(1-t)t^2 \end{bmatrix} \\ &= (1-t)^3 \begin{bmatrix} -1 \\ 0 \end{bmatrix} + 3(1-t)^2t \begin{bmatrix} 0 \\ 1 \end{bmatrix} + 3(1-t)t^2 \begin{bmatrix} 0 \\ -1 \end{bmatrix} + t^3 \begin{bmatrix} 1 \\ 0 \end{bmatrix}. \end{aligned}$$

The polynomial curve is expressed in terms of a combination of points. We may compute $X(0.5) = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$

A cubic Bézier curve is defined by

$$X(t) = (1-t)^3 lb_0 + 3(1-t)^2t lb_1 + 3(1-t)t^2 lb_2 + t^3 lb_3,$$

where lb_i , the Bézier control points, form the Bézier polygon of the curve.

$$X(t) = B_0^3(t) \cdot lb_0 + B_1^3(t) \cdot lb_1 + B_2^3(t) \cdot lb_2 + B_3^3(t) \cdot lb_3.$$

↳ the cubic Bernstein polynomials.

Properties of Cubic Bézier Curves

1. Endpoint interpolation: $X(0) = lb_0$, $X(1) = lb_3$.
2. Symmetry: Two polygons lb_0, lb_1, lb_2, lb_3 and lb_3, lb_2, lb_1, lb_0 describe the same curve; but the directions are different.
3. Invariance under rotations:
4. Invariance under affine maps: If an affine map is applied to the control polygon, the curve is mapped by the same map.
5. Convex hull property: For $t \in [0, 1]$, the point $X(t)$ is in the convex hull of the control polygon.
6. Linear precision: If $lb_1 = \frac{2}{3}lb_0 + \frac{1}{3}lb_3$ and $lb_2 = \frac{1}{3}lb_0 + \frac{2}{3}lb_3$, then the curve $X(t) = (1-t)lb_0 + tlb_3$: linear interpolation.

o. For $t \notin [0, 1]$, $X(t)$ may not stay within the convex hull of the control polygon.

3.3 Derivatives

$$\begin{aligned}
 \mathbf{x}'(t) &= -3(1-t)^2 \mathbf{lb}_0 + [3(1-t)^2 - 6(1-t)t] \mathbf{lb}_1 \\
 &\quad + [6(1-t)t - 3t^2] \mathbf{lb}_2 + 3t^2 \mathbf{lb}_3 \\
 &= (1-t)^2 \cdot 3[\mathbf{lb}_1 - \mathbf{lb}_0] + 2(1-t)t \cdot 3[\mathbf{lb}_2 - \mathbf{lb}_1] + t^2 \cdot 3[\mathbf{lb}_3 - \mathbf{lb}_2] \\
 &= (1-t)^2 \cdot 3\Delta \mathbf{lb}_0 + 2(1-t)t \cdot 3\Delta \mathbf{lb}_1 + t^2 \cdot 3\Delta \mathbf{lb}_2 \\
 &\quad \hookrightarrow \text{the forward difference} \leftarrow \\
 &= 3 \left(B_0^2(t) \cdot \Delta \mathbf{lb}_0 + B_1^2(t) \cdot \Delta \mathbf{lb}_1 + B_2^2(t) \cdot \Delta \mathbf{lb}_2 \right)
 \end{aligned}$$

$\hookrightarrow$ the quadratic Bernstein basis functions

- o. For parametric curves, "derivative curves" produce vectors rather than points.
- o. The coefficients are the difference vectors of the polygon, scaled by 3, the degree of the curve.
- o. $\mathbf{x}'(0) = 3\Delta \mathbf{lb}_0$, $\mathbf{x}'(1) = 3\Delta \mathbf{lb}_2$

3.4 The de Casteljau Algorithm

$$\left\{ \begin{aligned} \mathbf{lb}_0'(t) &= (1-t)\mathbf{lb}_0 + t\mathbf{lb}_1 \\ \mathbf{lb}_1'(t) &= (1-t)\mathbf{lb}_1 + t\mathbf{lb}_2 \\ \mathbf{lb}_2'(t) &= (1-t)\mathbf{lb}_2 + t\mathbf{lb}_3 \end{aligned} \right\} \Rightarrow \left\{ \begin{aligned} \mathbf{lb}_0^2(t) &= (1-t)\mathbf{lb}_0'(t) + t\mathbf{lb}_1'(t) \\ \mathbf{lb}_1^2(t) &= (1-t)\mathbf{lb}_1'(t) + t\mathbf{lb}_2'(t) \end{aligned} \right\}$$

$$\Rightarrow \underline{\underline{\mathbf{lb}_0^3(t) = (1-t)\mathbf{lb}_0^2(t) + t\mathbf{lb}_1^2(t)}} \\
 \mathbf{x}(t)$$

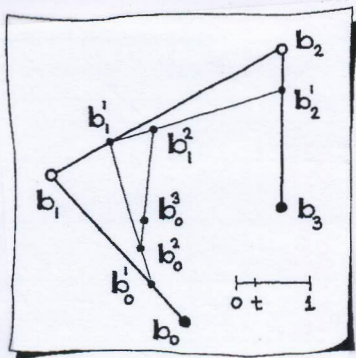
A convenient schematic tool for the algorithm

$$\left\{ \begin{array}{l} \mathbf{lb}_0 \searrow \mathbf{lb}_0'(t) \searrow \mathbf{lb}_0^2(t) \searrow \mathbf{lb}_0^3(t) \\ \mathbf{lb}_1 \searrow \mathbf{lb}_1'(t) \searrow \mathbf{lb}_1^2(t) \searrow \mathbf{lb}_1^3(t) \\ \mathbf{lb}_2 \searrow \mathbf{lb}_2'(t) \searrow \mathbf{lb}_2^2(t) \searrow \mathbf{lb}_2^3(t) \\ \mathbf{lb}_3 \searrow \mathbf{lb}_3'(t) \searrow \mathbf{lb}_3^2(t) \searrow \mathbf{lb}_3^3(t) \end{array} \right.$$

- o. In the implementation, $\mathbf{lb}_0'$ is calculated and loaded into $\mathbf{lb}_0$ since $\mathbf{lb}_0$ is never needed.
- $\Rightarrow$ 1D array of control points is sufficient!

$$\text{o. } \mathbf{x}'(t) = 3 [\mathbf{lb}_1^2(t) - \mathbf{lb}_0^2(t)] :$$

The derivative is essentially a byproduct of point evaluation!



Sketch 27.

The de Casteljau algorithm.

3.5 Subdivision

- o. Two polygons $lb_0, lb'_0, lb''_0, lb'''_0$ and $lb'''_0, lb''_1, lb'_1, lb_1$ define two segments corresponding to $[0, t]$ and $[t, 1]$, respectively.
- o. Subdivision at $t=0.5$ splits the curve at the parameter midpoint, but the two arcs are not of equal length.
- o. Subdivision may be repeated: Each of the two new control polygons may be subdivided, ... The resulting sequence of control polygons converges to the curve.
- o. Another application is the intersection of a curve with a line.
 1. Find the AABB (axis aligned bounding box) of the polygon.
 2. If no intersection between the AABB and the line, EXIT.
 3. Else if the AABB is smaller than ϵ , report the center of the AABB.
 4. Else, subdivide the curve at $t=0.5$ into two and repeat the same procedure to each segment.
- o. The curve-curve intersection can be done in a similar way. In this case, the curve with a bigger AABB is subdivided.

4.5 Degree Elevation

a. A Bézier curve of degree n may be represented as a Bézier curve of degree $(n+1)$.

Ex

$X(t) = (1-t)^2 b_0 + 2(1-t)t b_1 + t^2 b_2$: a quadratic curve.

Multiplying by $1 = [(1-t) + t]$, we get

$$\begin{aligned} X(t) &= [(1-t)^3 + (1-t)^2 t] b_0 + 2[(1-t)^2 t + (1-t)t^2] b_1 \\ &\quad + [(1-t)t^2 + t^3] b_2 \\ &= (1-t)^3 b_0 + 3(1-t)^2 t \left[\frac{1}{3} b_0 + \frac{2}{3} b_1 \right] \\ &\quad + 3(1-t)t^2 \left[\frac{2}{3} b_1 + \frac{1}{3} b_2 \right] + t^3 b_2. \end{aligned}$$

$$\therefore X(t) = B_0^3(t) b_0 + B_1^3(t) \left[\frac{1}{3} b_0 + \frac{2}{3} b_1 \right] + B_2^3(t) \left[\frac{2}{3} b_1 + \frac{1}{3} b_2 \right] + B_3^3(t) b_2.$$

Ex 4.2

$$X(t) = (1-t)^2 b_0 + 2(1-t)t b_1 + t^2 b_2,$$

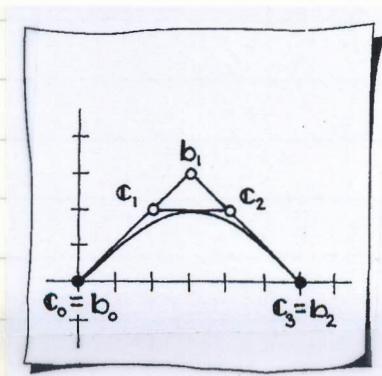
$$\text{where } b_0 = \begin{bmatrix} 0 \\ 0 \end{bmatrix}, b_1 = \begin{bmatrix} 3 \\ 3 \end{bmatrix}, b_2 = \begin{bmatrix} 6 \\ 0 \end{bmatrix}.$$

Degree elevation will produce

$$X(t) = (1-t)^3 c_0 + 3(1-t)^2 t c_1 + 3(1-t)t^2 c_2 + t^3 c_3,$$

$$\text{where } c_0 = b_0 = \begin{bmatrix} 0 \\ 0 \end{bmatrix}, c_3 = b_2 = \begin{bmatrix} 6 \\ 0 \end{bmatrix}$$

$$c_1 = \frac{1}{3} b_0 + \frac{2}{3} b_1 = \begin{bmatrix} 2 \\ 2 \end{bmatrix}, c_2 = \frac{2}{3} b_1 + \frac{1}{3} b_2 = \begin{bmatrix} 4 \\ 2 \end{bmatrix}.$$



$$\rightarrow 2 \times \frac{2!}{2! \times 12!}$$

Degree elevation of a Bézier curve of degree n to a Bézier curve of degree $(n+1)$:

$$\begin{cases} C_0 = 1b_0 \\ \vdots \\ C_i = \frac{i}{n+1} 1b_{i-1} + (1 - \frac{i}{n+1}) 1b_i \\ \vdots \\ C_{n+1} = 1b_n \end{cases}$$

$$\Rightarrow \begin{bmatrix} 1 & & & & \\ * & * & & & \\ & \ddots & & & \\ & & * & * & \\ & & & & 1 \end{bmatrix} \begin{bmatrix} 1b_0 \\ \vdots \\ 1b_n \end{bmatrix} = \begin{bmatrix} C_0 \\ \vdots \\ C_{n+1} \end{bmatrix}$$

$\hookrightarrow (n+2) \times (n+1)$ matrix
 $\underline{DB = C}$

- The process of degree elevation may be repeated. The resulting sequence of central polygons converges to the curve. However, convergence is too slow.

Ex 4.3

For $n=2$,

$$\begin{bmatrix} 1 & 0 & 0 \\ 1/3 & 2/3 & 0 \\ 0 & 2/3 & 1/3 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1b_0 \\ 1b_1 \\ 1b_2 \end{bmatrix} = \begin{bmatrix} C_0 \\ C_1 \\ C_2 \\ C_3 \end{bmatrix}$$

4.6 Degree Reduction

- o. The inverse process of degree reduction is more important. Some CAD systems allow degrees up to 40, others use cubic curves. Reducing a curve of degree 40 to cubic is non-trivial. In practice, several cubic segments will be needed, involving an interplay between subdivision and degree reduction.
- o. Degree reduction approximates a curve of degree $(n+1)$ by a curve of degree n . To approximate the solution of $D^T B = C$, we solve $D^T D B = D^T C$.
- o. The matrix $D^T D$ is independent of the given data, but dependent only on n . To solve many degree reduction problems, we store the LU factorization of $D^T D$.

Ex 4.4

For $n+1=3$, $D^T D = \frac{1}{9} \begin{bmatrix} 10 & 2 & 0 \\ 2 & 8 & 2 \\ 0 & 2 & 10 \end{bmatrix}$

For the degree-elevated cubic curve $x(t)$ with $c_0 = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$, $c_1 = \begin{bmatrix} 2 \\ 2 \end{bmatrix}$, $c_2 = \begin{bmatrix} 4 \\ 2 \end{bmatrix}$, $c_3 = \begin{bmatrix} 6 \\ 0 \end{bmatrix}$, we get

$$D^T C = \frac{1}{3} \begin{bmatrix} 2 & 2 \\ 12 & 8 \\ 22 & 2 \end{bmatrix}$$

corresponds to the x -components corresponds to the y -components

$$\Rightarrow B = (D^T D)^{-1} (D^T C) = \begin{bmatrix} 0 & 0 \\ 3 & 3 \\ 6 & 0 \end{bmatrix}$$

$$\therefore b_0 = \begin{bmatrix} 0 \\ 0 \end{bmatrix}, b_1 = \begin{bmatrix} 3 \\ 3 \end{bmatrix}, b_2 = \begin{bmatrix} 6 \\ 0 \end{bmatrix}.$$

- o. In general, the degree-reduced curve may not pass through the original curve endpoint c_0 and c_{n+1} .